# Stochastic Channel Modeling for Railway Tunnel Scenarios at 25 GHz

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and system-level design of the communication system

Keywords: MHN, Millimeter wave channel, Railway

communication, Ray tracing simulation, Stochastic

More people prefer using rail traffic for travel or for commuting owing to its convenience and flexibility. The railway scenario has become an important communication scenario in the fifth generation era. The communication system should be designed to support high-data-rate demands with connectivity at a high mobility. In this paper, the channel characteristics are studied and modeled for the railway tunnel scenario with straight and curved route shapes. On the basis of measurements using the "Mobile Hotspot Network" system, a threedimensional ray tracer (RT) is calibrated and validated for the target scenarios. More channel characteristics are explored via RT simulations at 25.25 GHz with a 500-MHz bandwidth. The key channel parameters are extracted, provided, and incorporated into a 3rd-**Generation-Partnership-Project-like stochastic channel** generator. The necessary channel information can be practically realized, which can support the link-level

I. Introduction

in similar scenarios.

channel modeling.

Currently, a growing number of people prefer to take rail traffic for traveling and commuting because of the comfortable experience and convenience that it provides. In order to meet the goals of efficiency, safety, and convenience, rail traffic is expected to be "smart" in the fifth generation (5G) era. The railway infrastructure, trains, travelers, and goods will be increasingly interconnected. Thus, rail-traffic communication has become an increasingly important topic, and seamless high-data-rate wireless connectivity Consequently, railway communications are required to evolve from handling only the critical signaling applications to support various high-data-rate applications [1], [2]. In order to realize this vision, the millimeter wave (mmWave) band has become important to overcome spectrum scarcity, and many efforts have been carried out to develop novel technologies such as multiple-inputmultiple-output (MIMO) beamforming [3]-[6], resource allocation, and multiple access. The 5GCHAMPION project [7], funded by the H2020 Europe-Korea collaborative program, aims to develop key enabling technologies for a proof-of-concept environment to be showcased at the 2018 Winter Olympics in PyeongChang, Korea. One of the key applications is to provide a highmobility broadband connection via a 5G mmWave highcapacity backhaul in the range of 24 GHz to 28 GHz. The

pISSN: 1225-6463. eISSN: 2233-7326

Manuscript received Sept. 15, 2017; revised Nov. 21, 2017; accepted Nov. 30, 2017.

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Electronics and Telecommunication Research Institute (ETRI), as a member of the 5GCHAMPION project, prototyped a new wireless communication system named "Mobile Hotspot Network (MHN)," which works in the range of 24 GHz to 30 GHz with 125-MHz, 250-MHz, 500-MHz, and 1-GHz bandwidths. It targets the support of services with a data rate of gigabits per second with a speed over 400 km/h [8], and several trials have been carried out in the Seoul Subway.

Standardization organizations are becoming active in the promotion of the priority in standardizing mmWave highspeed railway (HSR) communication technologies as well. In IEEE 802.15, the "High Rate Rail Communications" interest group was founded in 2014 to invite proposals and studies on broadband HSR communications. In 2016, the Macro + Relay deployment for the HSR scenario was agreed to be included in the 3rd Generation Partnership Project (3GPP) evaluation [9]–[11]. The working frequency is around 30 GHz, and the bandwidth is above 100 MHz. Each baseband unit is attached to three remote radio heads (RRHs). RRHs are uniformly deployed along the two rail tracks. The suggested distance from the RRH to the rail track is 5 m. MIMO systems with a unidirectional beam or bidirectional beam are recommended to compensate the high attenuation of mmWave band propagation. A correct understanding of the mmWave propagation channel characteristics in railway scenarios is mandatory to effectively support the design and evaluation of communication systems [12]. However, the mmWave band channel has been explored mainly for urban indoor and outdoor scenarios [13]–[16]. According to [17], the railway environments are divided into 19 scenarios on the basis of a review of four different HSR lines and eight HSR stations. Five applications are defined in [1], [2] from the viewpoint of propagation and wireless channels, including the train-to-infrastructure, intercar, intracar, inside-the-station, and infrastructure-toinfrastructure communications. The route shapes are also very important to the mobility and communication design. Straight and curved route shapes are typical in railways. However, most of the current studies focus on the straight route owing to a lack of measurements of the curved route. The works on existing standardized channel modeling rarely provide dedicated parameters for railway scenarios [18], [19].

In this study, the channel characteristics of tunnel scenarios are studied and modeled. Measurements are conducted in the 5G mmWave band in Seoul Subway Line 8 for both straight and curved routes. The 3D environments of the measurement campaign are modeled, and a ray tracer (RT) is calibrated and leveraged with the measurements to

explore more channel characteristics. The key time-variant channel parameters and their correlations are modeled. The stochastic channels are realized on the basis of a 3GPP-like channel generator. The validated results indicated that the 3GPP-like framework is suitable for describing highmobility scenarios. With the provided parameters, researchers and engineers can practically realize 3GPP-like channels to evaluate the designed communication technology in similar scenarios.

The remainder of this paper is organized as follows: The measurements and RT calibration are introduced in Section II. The channel parameters are analyzed and modeled in Section III. The conclusions are drawn in Section IV.

# II. Measurement Campaign and Ray-Tracer Calibration

#### 1. Measurement Campaign

An MHN Radio Unit (mRU), which is also called a transmitter (Tx) in this work, is installed on the side wall of the tunnel (see Fig. 1(a)), and the MHN Terminal Equipment (mTE), which is also called a receiver (Rx), is installed at the middle of the front window in the cab. The heights of the mRUs and mTE are 3.2 m and 3.0 m, respectively. The shortest two-dimensional distance between an mRU and the mTE is 2.8 m. The antenna used for both the mRUs and mTE is an 8 × 8 patch array antenna, as shown in Fig. 1(b). The measurements are conducted by installing the MHN test bed in Seoul Subway Line 8 from Jamsil station to a place after Songpa station, as shown in Fig. 1(c). A curved route is connected to a straight route in the measurement campaign. The radius of curvature of the tunnel is around 500 m. The lengths of the curved route and the straight route are 600 m and around 1,700 m, respectively. The half-power beam width (HPBW) is 8°, and the antenna gain is 22 dBi with vertical-horizontal dual polarization, as shown in Fig. 2. The main lobes of both the mRUs and mTE are pointed at each other, and handover occurs when the train is near an mRU. Three mRUs (mRU1, mRU2, and mRU3) are installed in the curved route with distances less than 300 m to guarantee a stable communication link under possible non-line-of-sight conditions. Only two mRUs (mRU4 and mRU5) are installed on the straight route, and the largest tested link distance is 1,180 m at mRU5.

#### 2. Environmental Modeling

As shown in Fig. 3, the cross section of the tunnel is a rectangle with pylons in the middle that separate the

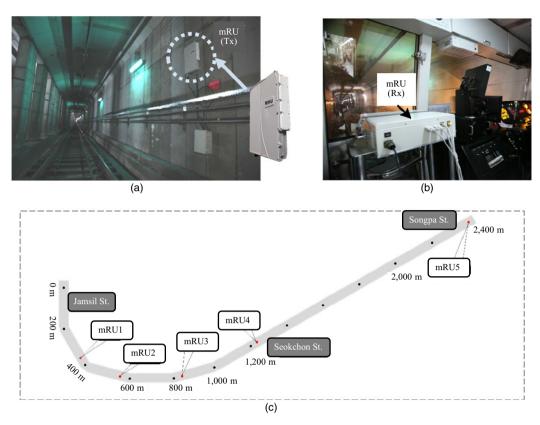


Fig. 1. Measurement campaign: (a) MHN test bed mRU (Tx) installation details, (b) MHN test bed mTE (Rx) installation details, and (c) measurement along Seoul Subway Line 8.

two-way tracks. The width of the tunnel is 13.7 m, and the height is 7.1 m. Figure 4 shows the constructed straight and curved tunnel models for the RT simulation. The side wall and pylons are made of concrete, the tracks are made of metal, and the train is made of metal (train body) and glass (windows). The lengths of the two models are greater than 1,200 m, which are longer than the measured length.

#### 3. Ray-Tracer Calibration

The deployment and configuration of the mRUs and mTE in the RT are the same as those in the measurement campaign. A calibration algorithm based on a simulated annealing method [21], [22] is employed to reduce the error by seeking the appropriate material parameters. The calibrated dielectric parameters and scattering coefficients of the directive scattering model [23] of concrete, glass, and metal are provided in Table 1; note that the calibrated transmission loss of glass is 833.33 dB/m (the equivalent attenuation with a thickness of 6 mm is 5.0 dB). Figure 5 shows the progress of the calibration. As the number of iterations increases, the calibration error decreases and

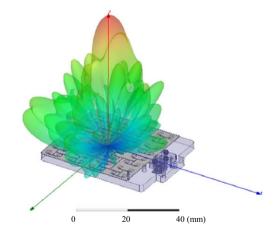


Fig. 2. Antenna pattern of mRU and mTE (V-polarization): HPBW = 8°, Gain = 22 dBi.

saturates after the 4th iteration. The received power of snapshot s is expressed as  $P_{\rm rx}(s) = \sum_{\tau=0}^{\tau_{\rm max}} |h(s,\tau)|^2$ , and Fig. 6 compares the cumulative distribution functions (CDFs) of the error of  $P_{\rm rx}$  (mW) before and after RT calibration. The mean absolute errors of the calibrated RT are  $4.2 \times 10^{-5}$  mW (straight route) and  $5.1 \times 10^{-5}$  mW

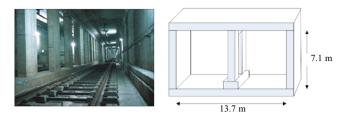
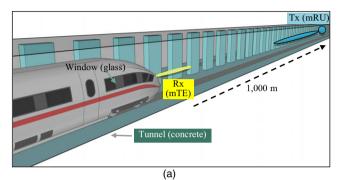


Fig. 3. Cross section of Seoul Subway Line 8 [20].



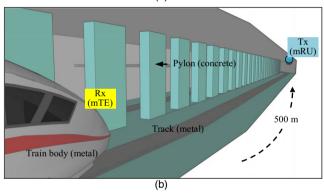


Fig. 4. (a) Straight and (b) curved tunnel scenarios.

Table 1. Material parameters.

Material name	$\epsilon'_r$	$\epsilon''_r$	A (dB/m)	S	α
Concrete	5.310	0.307	Not involved	0.0011	40
Glass	6.270	0.149	833.33	$6.27 \times 10^{-4}$	91
Metal	1.000	10 <sup>7</sup>	INF	0	0

(curved route); the standard deviation (STD) of the absolute errors in milliwatts are  $6.3 \times 10^{-5}$  and  $7.6 \times 10^{-5}$ , respectively. Thus, the calibrated RT results match the measurements well. Thereafter, intensive reliable RT simulations are conducted to practically explore more characteristics (azimuth/elevation angular spreads, omnidirectional channel characteristics) that could not be captured in the measurements. Figure 7

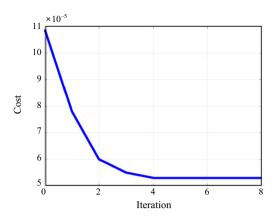


Fig. 5. Progress of the calibration results.

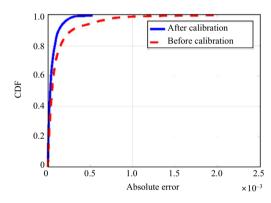


Fig. 6. CDF of the absolute errors before and after calibration.



Fig. 7. Rays traced for the straight and curved tunnels.

shows the transmitted and reflected rays traced for the curved tunnel.

# III. Simulation and Analysis of the Results

The MHN system works from 24 GHz to 30 GHz and supports a maximum bandwidth of 1 GHz. Recently, the Korean government released a regulation that the total effective isotropic radiated power should be smaller than 36 dBm, and the allocated frequency is 25 GHz to 25.5 GHz, which is lower than that in the measurements. To re-evaluate the system performance, accurate channels are needed for straight and curved routes with new parameters. RT simulations are conducted at 25.25 GHz with omnidirectional antennas at the Tx and Rx. As most

services have high requirements for the downlink in practice, the channel propagation and characteristics are analyzed by considering an mRU as the Tx and the mTE as the Rx in this work. The travel distance of the Rx is 1,000 m for the straight route and 350 m for the curved route. The distance between the Tx and the track center is 2.8 m. The snapshot sampling interval is 0.1 m. Thus, the total numbers of snapshots are 10,001 for the straight-route scenarios and 5,001 for the curved-route scenarios. Up to the 10th order of reflection, scattering and transmission are considered in the simulation.

#### 1. Path-Loss Model

Figure 8 shows how the path loss PL varies with the Tx–Rx distance d. The "A-B" model is employed in this work to fit the PL:

$$PL = A\log 10(d) + B + X_{\sigma},\tag{1}$$

where d is the distance between the Tx and the Rx, A is the slope, B is the intercept, and  $X_{\sigma}$  is the shadow fading (SF), which can be expressed as a zero-mean Gaussian random variable with an STD of  $\sigma$ . The fitting results are compared in Fig. 8 as well. As can be seen, a breakpoint at a distance  $d_{\rm bp}$  exists in both scenarios. When  $d \leq d_{\rm bp}$ , the region is defined as a near region. On the contrary, the far region is where  $d > d_{bp}$ . The extracted parameters are provided in Table 2.  $d_{bp}$  of the straight tunnel is five times that of the curved tunnel. In both scenarios,  $A_{near}$  is less than  $A_{far}$ . It is noteworthy that the train body, which is made of metal, blocks the direct transmission path at the very beginning of the near region. Thus, only the reflected and scattered rays can reach the Rx, which results a great difference between the simulated path loss and the freespace path loss. In the far region, the path loss in the curved tunnel is more severe than that in the straight tunnel, and  $A_{\text{curved}}$  is more than two times  $A_{\text{straight}}$ .  $\sigma_{\text{curved}}$ is smaller than  $\sigma_{\text{straight}}$  in both the near and far regions. The correlated distance of SF is defined as  $\lambda_{SF}$ , and the units are meters.  $\lambda_{SF}$  of the near region is smaller than that

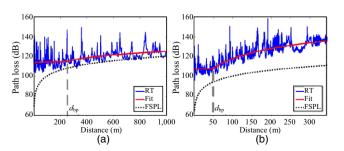


Fig. 8. Path losses of both scenarios: (a) path loss of the straight tunnel and (b) path loss of the curved tunnel.

Table 2. Extracted parameters for the PL.

PL	Straight tunnel $(d_{bp} = 257.2 \text{ m})$		Curved tunnel $(d_{bp} = 50 \text{ m})$		
	Near	Far	Near	Far	
A	0.64	16.50	0	33.40	
В	113.56	76.06	107.76	51.45	
$\sigma$ (dB)	5.93	4.96	4.53	4.83	
$\lambda_{\rm SF}$ (m)	1.10	1.70	1.00	1.10	

of the far region, and  $\lambda_{SF}$  of the curved tunnel is at least four times shorter than that of the straight tunnel. This observation indicates that the variation in the straight tunnel is less than that of the curved tunnel.

#### 2. Delay Spread and Rician K-Factor

Figure 9 shows the CDFs of the root-mean-square (RMS) delay spreads (DSs)  $\sigma_{\tau}$  of both scenarios.  $\sigma_{\tau}$  can be fitted by a lognormal distribution function (Table 3). In the straight tunnel, the mean RMS delay spread in the near region is larger than in the far region. In the curved tunnel, the values of  $\sigma_{\tau}$  for the near region and far region are similar and are fitted with the same model. The mean value and the range of variation of the straight tunnel are smaller than those of the curved tunnel. A Rician distribution indicates the presence of a specular dominant component in the channel over other very weak paths, and its probability density function (PDF) is expressed as

$$Px(x) = \frac{x}{\sigma_n^2} e^{-\frac{x^2 + A^2}{2\sigma_n^2}} I_0\left(\frac{Ax}{\sigma_n^2}\right),\tag{2}$$

$$K = 10\log 10 \left(\frac{A^2}{2\sigma_n^2}\right),\tag{3}$$

where  $I_0$  is the modified Bessel function of the first kind and zeroth order, A is the amplitude of the

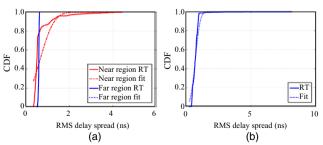


Fig. 9. Delay spreads of both scenarios: (a) DS of the straight tunnel and (b) DS of the curved tunnel.

Table 3. Extracted parameters for the DS.

DS	Straigh	Curved	
DS	Near	Far	tunnel
Mean log10 (ns)	-9.19	-9.24	-9.14
$\sigma_{ m DS} \log 10  ( m ns)$	-9.29	-10.67	-9.53
$\lambda_{\mathrm{DS}}\left(\mathrm{m}\right)$	6.80	20.30	4.60
$r_{ m DS}\left({ m m} ight)$	2.83	2.83	2.57

dominant path, and  $\sigma_n$  is the STD of all other weak path amplitudes. The amplitudes are computed by using the peak values of the channel impulse responses. The Rician K-factor (KF) is expressed by (3). The CDFs are compared in Fig. 10, and the fitting results are summarized in Table 4. The mean KFs of both scenarios are greater than 24 dB. In the far region of the straight tunnel, the mean value is greater than that in the near region. The mean KF of the curved-tunnel scenario is the lowest, indicating that multipath components contribute more significantly compared to the straight tunnel. The correlated distance  $\lambda_{\rm KF}$  of the curved tunnel is much less than that of the straight tunnel.

#### 3. Angular Domain

According to the 3GPP definition [24], the conventional angular spread (AS) calculation for the composite signal is given by

$$\sigma_{\text{AS}} = \sqrt{\frac{\sum_{n=1}^{N} \sum_{m=1}^{M} (\theta_{n,m,\mu})^{2} \cdot P_{n,m}}{\sum_{n=1}^{N} \sum_{m=1}^{M} P_{n,m}}},$$

where  $P_{n,m}$  is the power for the *m*th subpath of the *n*th path,  $\theta_{n,m,\mu}$  is defined as

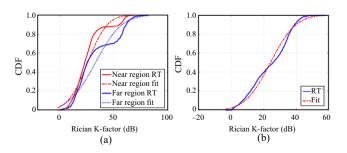


Fig. 10. Rician K-factors: (a) KF of the straight tunnel and (b) KF of the curved tunnel.

Table 4. Extracted parameters for the KF.

KF	Straigh	Curved	
KΓ	Near	Far	tunnel
Mean (dB)	25.70	32.95	24.02
$\sigma_{\mathrm{KF}}\left(\mathrm{dB}\right)$	14.23	19.15	12.24
$\lambda_{\mathrm{KF}}\left(\mathbf{m}\right)$	11.20	14.60	2.10

$$\theta_{n,m,\mu} = \begin{cases} 2\pi + (\theta_{n,m} - \mu_{\theta}) & \text{if} \quad (\theta_{n,m} - \mu_{\theta}) < -\pi \\ (\theta_{n,m} - \mu_{\theta}) & \text{if} \quad |\theta_{n,m} - \mu_{\theta}| \le \pi \\ 2\pi - (\theta_{n,m} - \mu_{\theta}) & \text{if} \quad (\theta_{n,m} - \mu_{\theta}) > \pi \end{cases},$$

 $\mu_{\theta}$  is defined as

$$\mu_{\theta} = \frac{\sum_{n=1}^{N} \sum_{m=1}^{M} \theta_{n,m} \cdot P_{n,m}}{\sum_{n=1}^{N} \sum_{m=1}^{M} P_{n,m}},$$

and  $\theta_{n,m}$  is the angle of arrival/departure of the *m*th subpath of the *n*th path. *m* is 1 for RT simulation results.

The RMS ASs of both scenarios are shown in Fig. 11. The fitting parameters are listed in Table 5. ASA, ASD, ESA, and ESD are the angular spreads of the azimuth angle of arrival (AoA), the azimuth angle of departure, the elevation angle of arrival (EoA), and the elevation angle of departure, respectively. The ASs of the straight tunnel in the far region are the smallest with the smallest variation.  $\lambda_{AS}$  of the far region of the straight route is the largest compared to the others (Table 6).

#### 4. Cross-Correlation between the Key Parameters

The cross-correlations are computed for the aforementioned parameters. Tables 7 and 8 summarize the parameters for the near and far regions of the

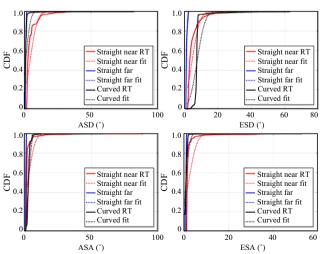


Fig. 11. CDFs of the ASs.

Table 5. Extracted parameters for the ASs.

ASD	Straigh	t tunnel	Curved
ASD	Near	Far	tunnel
Mean log10 (°)	0.63	$9.65 \times 10^{-4}$	0.02
$\sigma_{ m ASD} \log 10  (^{\circ})$	0.64	-0.52	0.44
$\lambda_{\mathrm{ASD}}$ (m)	6.00	19.40	2.90
	Ctraigh	t tunnal	G 1
ESD		t tunnel	Curved
	Near	Far	tunnel
Mean log10 (°)	0.65	0.03	0.87
$\sigma_{ m ESD} \log 10 (^{\circ})$	0.56	-0.38	0.57
$\lambda_{\rm ESD}$ (m)	2.90	17.50	4.80
ASA	Straigh	Curved	
ASA	Near	Far	tunnel
Mean log10 (°)	0.37	-0.04	0.47
$\sigma_{\rm ASA} \log 10  (^{\circ})$	0.62	-0.76	0.26
$\lambda_{ASA}$ (m)	6.95	19.90	4.00
ESA	Straigh	t tunnel	Curved
ESA	Near	Far	tunnel
Mean log10 (°)	0.28	-0.07	-0.07
σ <sub>ESA</sub> log10 (°)	0.47 -0.94		0.12

straight tunnel, respectively. The cross-correlation of the DS and SF is positive in both regions, whereas the correlation between the DS/SF and other parameters are negative. Further, the cross-correlations of the other parameters significantly increase in the far region. When the diversity of multipath components (MPCs) increases, the variation in the SF increases as well. When the DS increases/decreases, the multipath components are more/ less diverse in the time domain. The DS and SF are positively correlated, indicating that the SF is likely to vary with a similar trend as the DS. However, the angles are constrained within the narrow propagation region, and the range of ASs in the far region is less than that in the near region of the straight tunnel. Thus, the variations in the delays of rays barely influence the angles, especially in the far region of the straight tunnel. In the curved tunnel (see Table 8), the KF and SF are barely correlated with the other parameters. In both scenarios, the ASs are strongly correlated.

15.45

20.00

4.20

# 5. Polarization

 $\lambda_{ESA}$  (m)

The cross-polarization ratio (XPR) refers to the field received in the vertical (horizontal) copolarization relative

Table 6. Cross-correlation of the straight tunnel in the near region.

	DS	KF	SF	ASD	ASA	ESD	ESA
DS	1	0.52	0.20	0.87	0.76	0.83	0.78
KF		1	-0.12	0.65	0.23	0.64	0.21
SF			1	0.13	0.18	0.08	0.17
ASD				1	0.59	0.76	0.57
ASA					1	0.53	0.92
ESD						1	0.61
ESA							1

Table 7. Cross-correlation of the straight tunnel in the far region.

	DS	KF	SF	ASD	ASA	ESD	ESA
DS	1	-0.65	0.11	-0.75	-0.68	-0.72	-0.64
KF		1	0.01	0.96	0.98	0.89	0.99
SF			1	-0.01	-0.01	-0.03	0.01
ASD				1	0.97	0.94	0.96
ASA					1	0.94	0.99
ESD						1	0.89
ESA							1

Table 8. Cross-correlation of the curved tunnel.

	DS	KF	SF	ASD	ASA	ESD	ESA
DS	1	0.12	0	0.45	0.84	0.69	0.57
KF		1	-0.03	0.07	-0.17	0.05	0.01
SF			1	0.03	-0.03	0.02	0.07
ASD				1	0.47	0.52	0.67
ASA					1	0.60	0.69
ESD						1	0.47
ESA					·		1

to the field transmitted in the vertical polarization (horizontal) and received horizontal polarization (vertical). The XPR is expressed as

 $XPR = 20\log 10 \left(\frac{E_{co}}{E_{cross}}\right).$ 

The XPRs are fitted as a normal distribution (Fig. 12), and Table 9 summarizes the parameters. The smallest XPRs are negative in both scenarios with a probability of less than 20%, indicating that the copolarization configuration outperforms the cross-polarization configuration with a very large chance. The depolarization is the most severe in the

far region of the straight tunnel, as the mean XPR and minimum XPR are the smallest compared with the others. Thus, a dual polarization configuration at the Tx and Rx is suggested.

### 6. Clustering

The clustering procedure is realized by using a K-power-means algorithm clustering algorithm by considering the power, delay, AoA, and EoA. Twenty clusters are generated for both scenarios. The per-cluster parameters are summarized in Table 10. The per-cluster parameters in the far region of the straight tunnel are the smallest compared to the others.

#### 7. Validation of the Channel Models

With all of the provided parameters in this work, stochastic channels can be generated by using a 3GPP-like channel generator. The QuaDRiGa channel generator [25], which includes all of the features of the 3GPP channel framework and supports the evolution of time-variant channel parameters, is used to realize and validate the channels. The deployment configuration and mobility patterns of the Tx and Rx are exactly the same as those in the RT, as shown in Fig. 13. Two segments

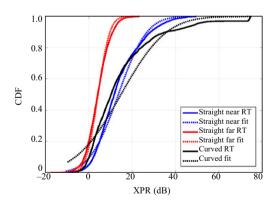


Fig. 12. Comparison of the XPRs.

Table 9. Extracted parameters for the XPR.

XPR	Straigh	Curved		
AFK	Near	Far	tunnel	
Mean (dB)	13.65	4.29	14.86	
$\sigma_{ m DS} \left( { m dB} \right)$	10.31	5.14	16.45	

are defined on the basis of the different values of  $d_{\rm bp}$  of the two scenarios. Examples of the values of PL of the generated channels are shown in Fig. 14. By running QuaDRiGa  $10^5$  times, the mean absolute error of PL is 2.5 dB, and the error in the PL coefficient is 0. The corresponding examples of the DS and KF are shown in Fig. 15. The mean absolute errors of the means and STDs are also 0. The validated parameters and the channel generator maintain consistency in the distribution of the large-scale parameters. As a result, the results of this work can be used to practically evaluate link/system-level technologies for similar tunnel scenarios.

#### IV. Conclusion

In this study, the channel characteristics are analyzed and modeled for railway tunnel scenarios in the mmWave band. Straight and curved route shapes are defined, and the 3D environment models are available online for free to download. Measurements are conducted inside the tunnel of a Seoul subway line. A 3D ray tracer is calibrated to ensure that the environment model and material parameters are practically close to reality. The transmission loss of the front window is 5 dB, and the dielectric parameters of the considered materials are obtained. The path loss, RMS delay spread, Rician K-

Table 10. Per-cluster parameters.

	Straigh	Curved	
	Near	Far	tunnel
SF (dB)	3	3.0	1.0
ASD (°)	2	0.5	0.5
ESD (°)	3	0.4	4.0
ASA (°)	1	0.4	2.0
ESA (°)	1	0.4	0.4

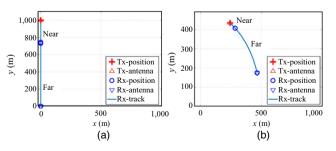


Fig. 13. Generated mobility patterns for both scenarios: (a) staight tunnel layout and (b) curved tunnel layout.

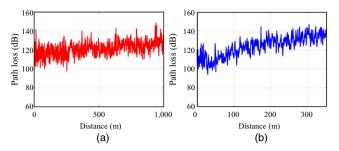


Fig. 14. Generated values of *PL* using the extracted parameters: (a) *PL* of the straight tunnel and (b) *PL* of the curved tunnel.

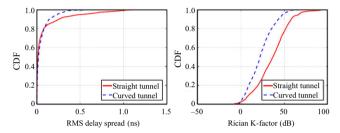


Fig. 15. Generated RMS delay spread and Rician K-factors for both scenarios using the extracted parameters.

factor, 3D angular spreads, and polarizations are extracted from the calibrated RT simulation, and the distributions and correlations are modeled. On the basis of a 3GPP-like channel modeling framework and the QuaDRiGa channel generator, the provided parameters are validated. The work of this paper indicates that the RT simulator can be integrated with channel measurements to analyze more characteristics. Moreover, the 3GPP-like channel framework and QuaDRiGa generator are suitable for describing high-mobility scenarios. With the provided parameters in this work, researchers and engineers can practically realize channels to evaluate the designed technology communication in similar scenarios. Moreover, the main observations from this work are summarized as follows:

- A break point exists in both scenarios, and d<sub>bp</sub> of the straight tunnel is larger than that of the curved tunnel. Thus, two sets of parameters should be extracted, and special attention should be paid when implementing a stochastic channel generator.
- The correlated distances of the key parameters in the far region are larger than those in the near region, meaning that the channel characteristics vary more drastically in the near region.
- Owing to the drastic variation in the multipath components, the *PL* slopes in the near region of both scenarios are approximately 0, which makes *PL* barely

- vary with the distance. In the far region, the curved tunnel suffers more path loss than that in the straight tunnel.
- The DS and SF are less correlated with the other parameters in the far region of the straight tunnel, whereas the other parameters are more correlated with each other. In the curved tunnel, the KF and SF are barely correlated with the other parameters. The ASs are strongly correlated in both scenarios.
- The copolarization configuration outperforms the crosspolarization configuration with more than 80% probability. The depolarization in the far region of the straight tunnel is the most severe compared to those of the others. Thus, a dual polarization configuration at the Tx and Rx is suggested.

In future work, different Tx/Rx configurations and multilink channel simulations will be explored. The influence of different configurations on link-level and system-level technologies will be evaluated.

## Acknowledgements

This work was supported by a grant from the Institute for Information & Communications Technology Promotion (IITP) funded by the Korean government (MSIT) (No. 2014-0-00282, Development of 5G Mobile Communication Technologies for Hyper-connected Smart Services).

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